



MINISTÉRIO DA CIÊNCIA E TECNOLOGIA
INSTITUTO NACIONAL DE PESQUISAS ESPACIAIS



Parallel version for the BRAMS with Runge-Kutta dynamical core

Luiz Flavio Rodrigues (*) Simone S. Tomita (*) Renata S. R. Ruiz (*)
Jairo Paneta (#) Saulo R. Freitas (##) Haroldo F. Campos Velho (*)

(*) INPE: National Institute for Space Research – Brazil

(#) ITA: Aeronautics Technological Institute – Brazil

(##) NASA: National Aeronautics and Space Administration – USA

Presentation outline

- Numerical time integration
 - Finite difference approximation for derivatives
 - ❖ Explicit method
 - ❖ Implicit method
 - ❖ Semi-implicit method
 - ❖ Implicit-explicit (IMEX) method
 - ❖ Higher order method
- BRAMS model
- Prediction under intense convection (CZSA)
- Final remarks

Numerical time integration

- Finite difference: advection/convection equation

$$\frac{\partial u}{\partial t} + a \frac{\partial u}{\partial x} = b \frac{\partial^2 u}{\partial x^2} + f(x, t)$$

$$u(x, 0) = u_0(x)$$

$$u(0, t) = u(L_x, t) = 0$$

$$U_i(t) \equiv u(x_i, t) \quad F_i(t) \equiv f(x_i, t) \quad \text{and} \quad x_i = x_{i-1} + \Delta x$$

Numerical time integration

- Finite difference: advection/convection equation

$$\left(\frac{\partial u}{\partial x}\right)_i = \frac{U_{i+1}(t) - U_{i-1}(t)}{2\Delta x} + O(\Delta x^2)$$

$$\left(\frac{\partial^2 u}{\partial x^2}\right)_i = \frac{U_{i+1}(t) - 2U_i(t) + U_{i-1}(t)}{\Delta x^2} + O(\Delta x^2)$$

$$\Delta x = L_x / N_x \quad \text{and} \quad N_x = 4$$

Numerical time integration

- Finite difference: advection/convection equation

$$\frac{dU_1(t)}{dt} + a \left[\frac{U_2(t) - U_0(t)}{2\Delta x} \right] = b \left[\frac{U_2(t) - 2U_1(t) + U_0(t)}{\Delta x^2} \right] + F_1(t)$$

$$\frac{dU_2(t)}{dt} + a \left[\frac{U_3(t) - U_1(t)}{2\Delta x} \right] = b \left[\frac{U_3(t) - 2U_2(t) + U_1(t)}{\Delta x^2} \right] + F_2(t)$$

$$\frac{dU_3(t)}{dt} + a \left[\frac{U_4(t) - U_2(t)}{2\Delta x} \right] = b \left[\frac{U_4(t) - 2U_3(t) + U_2(t)}{\Delta x^2} \right] + F_3(t)$$

Numerical time integration

- Finite difference: advection/convection matrix form

$$\frac{d\mathbf{U}(t)}{dt} + \mathbf{A}\mathbf{U} = \mathbf{B}\mathbf{U} + \mathbf{F}$$

$$\mathbf{U}(t) \equiv \begin{bmatrix} U_1(t) \\ U_2(t) \\ U_3(t) \end{bmatrix} \quad \mathbf{A} = \frac{a}{2\Delta x} \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 1 \\ 0 & -1 & 0 \end{bmatrix}$$

$$\mathbf{F}(t) \equiv \begin{bmatrix} F_1(t) \\ F_2(t) \\ F_3(t) \end{bmatrix} \quad \mathbf{B} = \frac{b}{\Delta x^2} \begin{bmatrix} -2 & 1 & 0 \\ 1 & -2 & 1 \\ 0 & 1 & -2 \end{bmatrix}$$

Numerical time integration

- Time integration: explicit method first order

$$\frac{d\mathbf{U}(t_n)}{dt} = \frac{\mathbf{U}^{n+1} - \mathbf{U}^n}{\Delta t} + O(\Delta t)$$

- Time integration: implicit method first order

$$\frac{d\mathbf{U}(t_{n+1})}{dt} = \frac{\mathbf{U}^{n+1} - \mathbf{U}^n}{\Delta t} + O(\Delta t)$$

Numerical time integration

- Time integration: semi-implicit (Crank-Nicolson) method

$$\frac{d\mathbf{U}(t_{n+1/2})}{dt} = \frac{\mathbf{U}^{n+1} - \mathbf{U}^n}{\Delta t} + O(\Delta t^2)$$

- Time integration: explicit (Leapfrog) second order

$$\frac{d\mathbf{U}(t_n)}{dt} = \frac{\mathbf{U}^{n+1} - \mathbf{U}^{n-1}}{2\Delta t} + O(\Delta t^2)$$

Numerical time integration

- Explicit Runge-Kutta 1st order

$$\mathbf{U}^{n+1} = \mathbf{U}^n - \Delta t [\mathbf{A}\mathbf{U}^n - \mathbf{B}\mathbf{U}^n - \mathbf{F}^n]$$

- Implicit Euler method

$$[\mathbf{I} + \Delta t (\mathbf{A} - \mathbf{B})] \mathbf{U}^{n+1} = \mathbf{U}^n + \Delta t \mathbf{F}^{n+1}$$

Numerical time integration

- Semi-implicit Crank-Nicolson method

$$\frac{d\mathbf{U}^{n+1/2}}{dt} \approx \frac{\mathbf{U}^{n+1} - \mathbf{U}^n}{\Delta t} = -\mathbf{A}\mathbf{U}^{n+1/2} + \mathbf{B}\mathbf{U}^{n+1/2} + \mathbf{F}^{n+1/2}$$

$$\mathbf{U}^{n+1/2} \approx \frac{1}{2} [\mathbf{U}^{n+1} + \mathbf{U}^n]$$

$$[2\mathbf{I} + \Delta t (\mathbf{A} - \mathbf{B})] \mathbf{U}^{n+1} = [2\mathbf{I} - \Delta t (\mathbf{A} - \mathbf{B})] \mathbf{U}^n + 2\Delta t \mathbf{F}^{n+1/2}$$

Numerical time integration

- Runge-Kutta 2nd order

$$\frac{U^{n+1} - U^n}{\Delta t} = -\mathbf{A}U^{n+1/2} + \mathbf{B}U^{n+1/2} + \mathbf{F}^{n+1/2}$$

$$U^{n+1/2} \approx \frac{1}{2} [U^{n+1} + U^n]$$

$$U_*^{n+1} = U^n - \Delta t [\mathbf{A}U^n - \mathbf{B}U^n - \mathbf{F}^n]$$

$$U^{n+1} = U^n - \frac{\Delta t}{2} [\mathbf{A} (U^n + U_*^{n+1}) - \mathbf{B} (U^n + U_*^{n+1}) - 2\mathbf{F}^{n+1/2}]$$

Numerical time integration

- Runge-Kutta 2nd order

$$\frac{U^{n+1} - U^n}{\Delta t} = G(U_{n+1/2}, t_{n+1/2})$$

$$U^{n+1} = U^n + (k_1 + k_2)/2 + O(\Delta t^2)$$

$$k_1 = \Delta t G(U^n, t_n)$$

$$k_2 = \Delta t G(U^n + k_1, t_n + \Delta t)$$

Numerical time integration

- Runge-Kutta 3rd order

$$\mathbf{U}^{n+1} = \mathbf{U}^n + (k_1 + 4k_2 + k_3)/6 + O(\Delta t^3)$$

$$k_1 = \Delta t \mathbf{G}(\mathbf{U}^n, t_n)$$

$$k_2 = \Delta t \mathbf{G}(\mathbf{U}^n + k_1/2, t_n + \Delta t/2)$$

$$k_3 = \Delta t \mathbf{G}(\mathbf{U}^n - k_1 + 2k_2, t_n + \Delta t)$$

Numerical time integration

- Implicit-Explicit (IMEX) method
- Equation: **non-stiff** and **stiff** components

$$\frac{d\mathbf{U}(t)}{dt} + \boxed{\mathbf{A}\mathbf{U}} = \boxed{\mathbf{B}\mathbf{U}} + \mathbf{F}$$

$$\frac{\mathbf{U}^{n+1} - \mathbf{U}^n}{\Delta t} = -\mathbf{A}\mathbf{U}^{n+1/2} + \mathbf{B}\mathbf{U}^{n+1/2} + \mathbf{F}^{n+1/2}$$

$$\frac{\mathbf{U}^{n+1} - \mathbf{U}^n}{\Delta t} = - \underbrace{\mathbf{A}\mathbf{U}^{n+1/2}}_{\text{Crank-Nicolson}} + \underbrace{\mathbf{B}\mathbf{U}^{n+1/2}}_{\text{Runge-Kutta 2nd}} + \mathbf{F}^{n+1/2}$$

Numerical time integration

- Implicit-Explicit (IMEX) method
- Equation: **non-stiff** and **stiff** components



IMEX SCHEMES FOR TIME INTEGRATION OF BURGERS' EQUATION

Antonio M. Zarzur

Haroldo F. Campos Velho

Stephan Stephany

Saulo R. Freitas

Numerical time integration

- Why other method for time integration?
 1. For enhancing the numerical precision
 2. To explore a new stability region: larger Δt !
 3. Larger $\Delta t \rightarrow$ for reducing the CUP-time to do a numerical prediction for finer spece resolution.

BRAMS model

BRAMS:

Brazilian developments to the **RAMS**

RAMS:

Regional **A**tmospheric **M**odeling **S**ystem

Developed by the Atmospheric Science Department of the Colorado State University (USA)

BRAMS is a meso-scale atmospheric simulator

BRAMS can represent different atmospheric processes on several space scales. The model employs a telescopic nested computer grid.

RAMS: Regional Atmospheric Model System

An atmospheric model able for simulating several types of the atmospheric flows, from large scale circulations up to microscale.

Starting its development at 70' s:

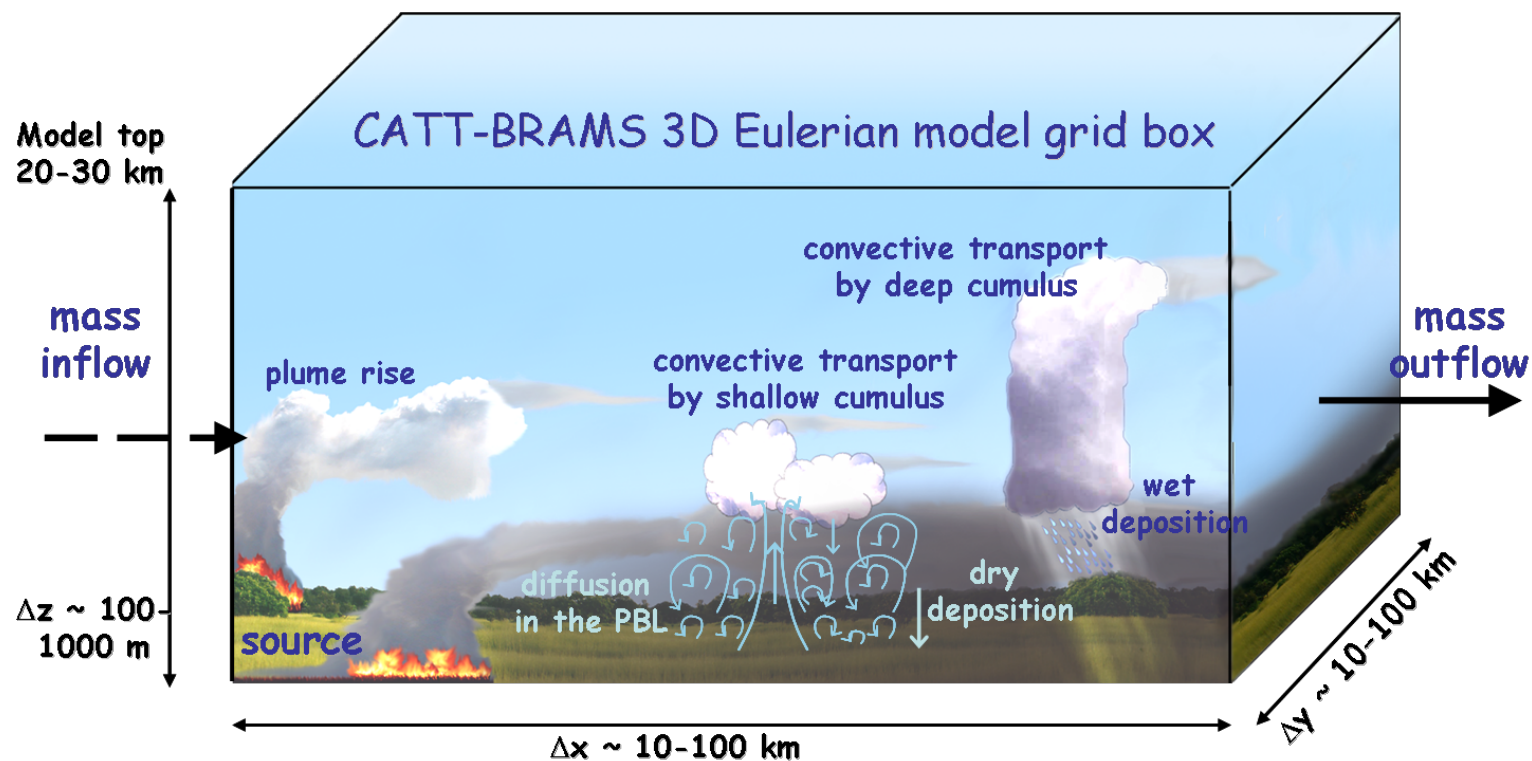
- Mesoscale model (Pielke, 1974)

- Model of clouds (Trípoli e Cotton, 1982)

First version (1986) \Rightarrow Department of Atmospheric Sciences
Colorado State University (CO, USA)

BRAMS: represented processes

BRAMS: Atmospheric simulation model



Eulerian transport model: CCATT-BRAMS atmospheric model

- in-line Eulerian transport model fully coupled to the atmospheric dynamics
- suitable for feedbacks studies
- tracer mixing ratio tendency equation

$$\frac{\partial \bar{s}}{\partial t} = \left(\frac{\partial \bar{s}}{\partial t} \right)_{adv} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{PBL\ turb} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{deep\ conv} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{shallow\ conv} + W_{PM\ 2.5} + R + Q_{plume\ rise}$$

- *adv* grid-scale advection
- *PBL turb* sub-grid transport in the PBL
- *deep conv* sub-grid transport associated to the deep convection including downdraft at cloud scale
- *shallow conv* sub-grid transport associated to the shallow convection
- *W* convective wet removal
- *R* sink term associated with dry deposition or chemical transformation
- *Q* source emission with plume rise sub-grid transport.

Eulerian transport model:

CCATT-BRAMS atmospheric model

- in-line Eulerian transport model fully coupled to the atmospheric dynamics
- suitable for feedbacks studies
- tracer mixing ratio tendency equation

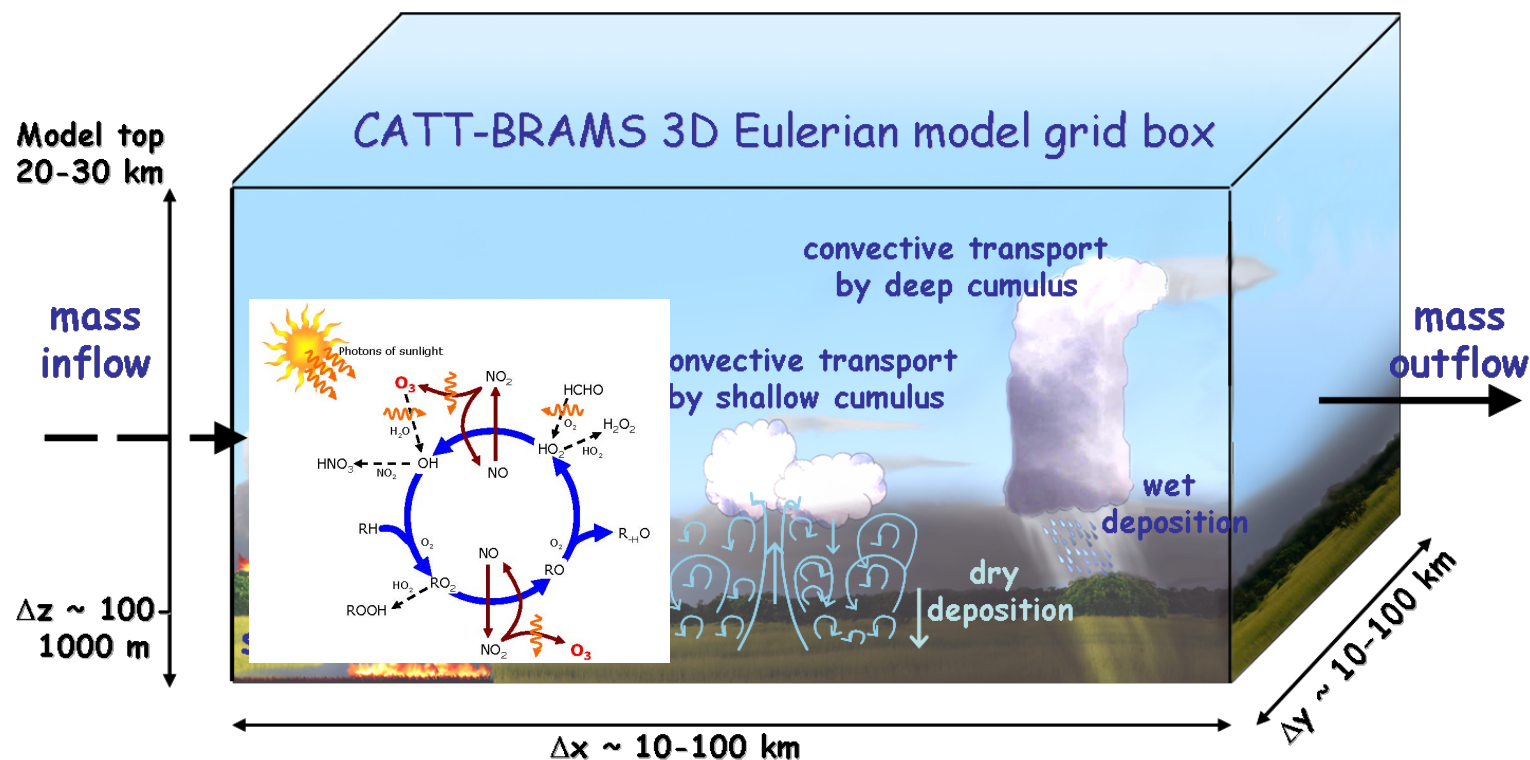
$$\frac{\partial \bar{s}}{\partial t} = \left(\frac{\partial \bar{s}}{\partial t} \right)_{adv} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{PBL\ turb} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{deep\ conv} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{shallow\ conv} + W_{PM2.5} + R +$$

$$+ Q_{plume\ rise} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{chemical\ reactions} + \left(\frac{\partial \bar{s}}{\partial t} \right)_{4dda}$$

- *adv* grid-scale advection
- *PBL turb* sub-grid transport in the PBL
- *deep conv* sub-grid transport associated to the deep convection including downdraft at cloud scale
- *shallow conv* sub-grid transport associated to the shallow convection
- *W* convective wet removal
- *R* sink term associated with dry deposition or chemical transformation
- *Q* source emission with plume rise sub-grid transport.
- *chem. reactions*
- *4dda* large-scale data assimilation via Newtonian relaxation (nudging).

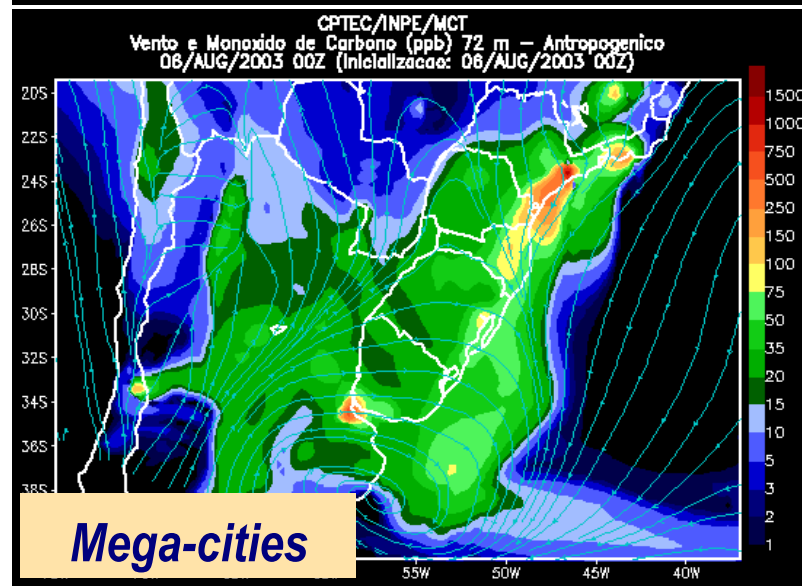
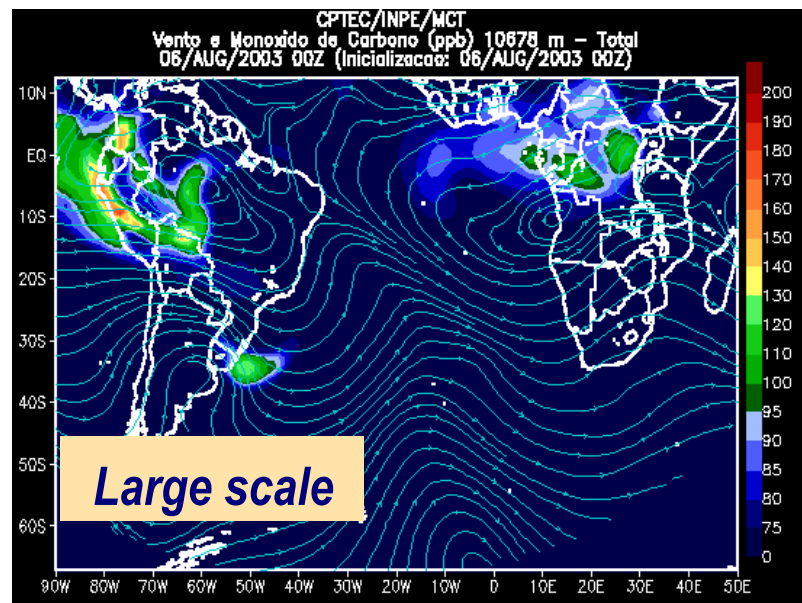
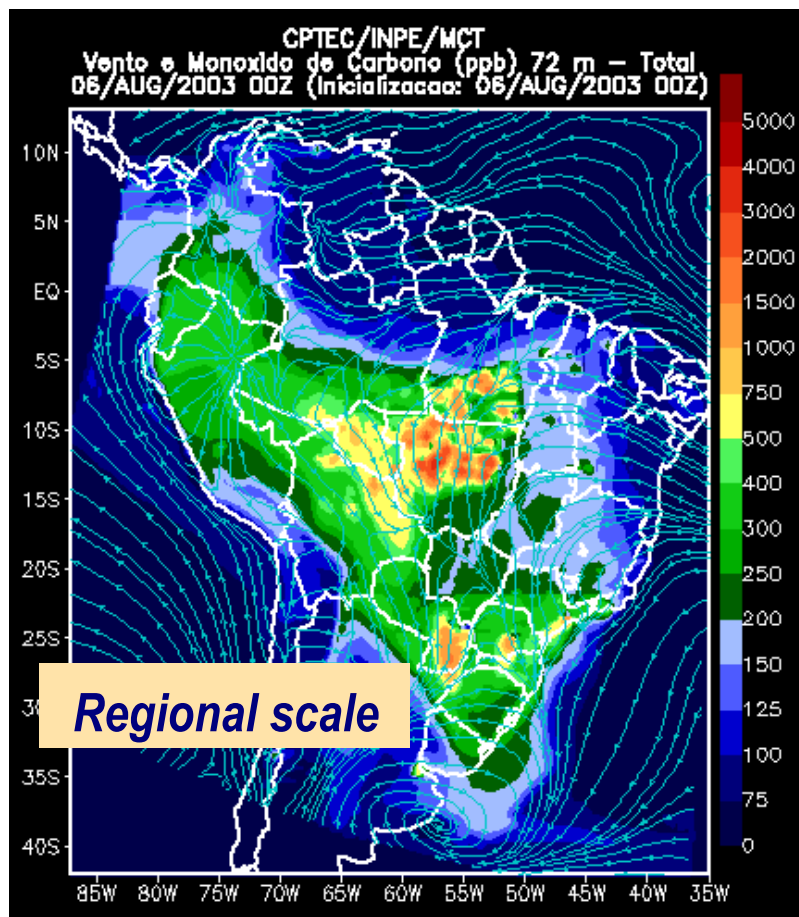
BRAMS: represented processes

BRAMS: Atmospheric simulation model
Chemical process



BRAMS environmental prediction

Pollutant emission by forest fires and urban-industries



BRAMS in Hybrid computers

Hybrid computing: CPU multi-core + GP-GPU

BRAMS: Atmospheric simulation model

Dynamical core: codified on CPU

Turbulence models: codified on GPU

- Smagorinsky (1963)
- Mellor-Yamada (1982)
- Taylor based approach (1998)



BRAMS in Hybrid computers

Hybrid computing: CPU multi-core + GP-GPU

Smagorinsky on GP-GPU

- CUDA (Nvidia) implementation
- OpenCL implementation



| OpenCL parcial code | time (ms) | CUDA parcial code (GPU-1) | time (ms) | CUDA parcial code (GPU-2) | Time (ms) |
|------------------------------|--------------|---|----------------|---|---------------|
| clCreateCommandQueue | 0.043 | cudaMalloc + cudaMemcpyAsync (CPU to GPU) | 52.397 + 0.353 | cudaMalloc + cudaMemcpyAsync (CPU to GPU) | 50.924+0.308 |
| clCreateBuffer | 0.012 | | | | |
| clCreateProgramWithoutSource | 0.337 | cuda_kernel_mxdefin_<<<...>>> >(,,) | 0.019 | cuda_kernel_mxdefin_<<<...>>> >(,,) | 0.016 |
| clSetKernelArg | 0.008 | | | | |
| clEnqueueNDRangeKernel | 0.045 | cudaMemcpy (GPU to CPU) | 0.319 | cudaMemcpy (GPU to CPU) | 0.571 |
| clEnqueueReadBuffer | 0.380 | cudaFree | 0.174 | cudaFree | 0.001 |
| clReleaseMemObject | 0.267 | | | | |
| Total | 1.263 | Total | 53.003 | Total | 51,820 |

BRAMS in Hybrid computers

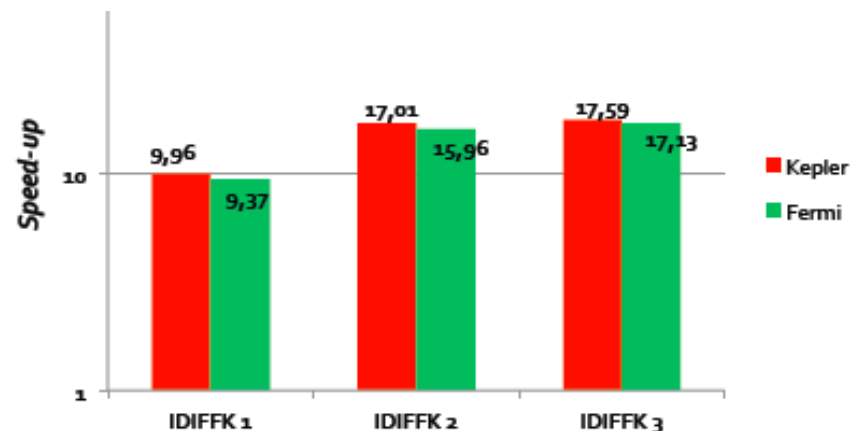
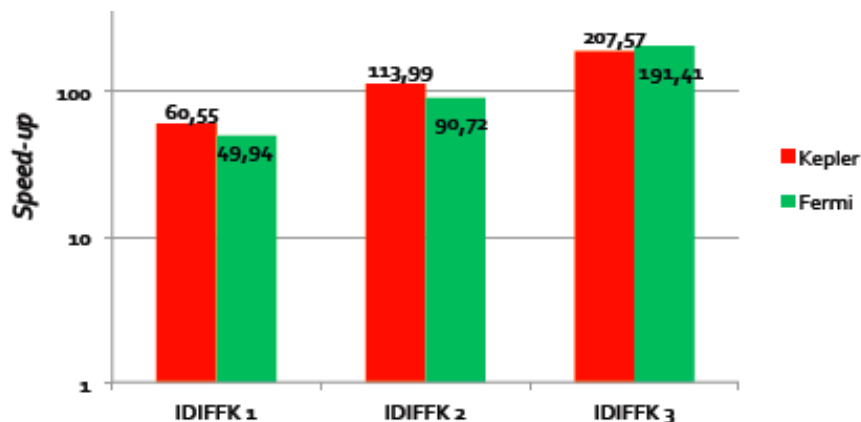
Hybrid computing: CPU multi-core + GP-GPU

Smagorinsky on GP-GPU

- CUDA (Nvidia) implementation
- OpenCL implementation



40 km (GPU: Fermi vs Kepler) 20 km



BRAMS – research in progress ...

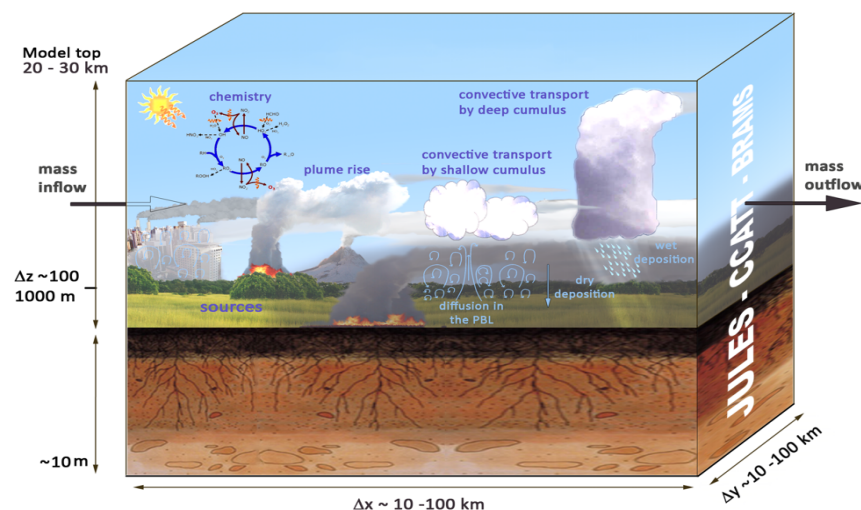
Adv. Geosci., 35, 123–136, 2013
www.adv-geosci.net/35/123/2013/
doi:10.5194/adgeo-35-123-2013
© Author(s) 2013. CC Attribution 3.0 License.

Advances in
Geosciences



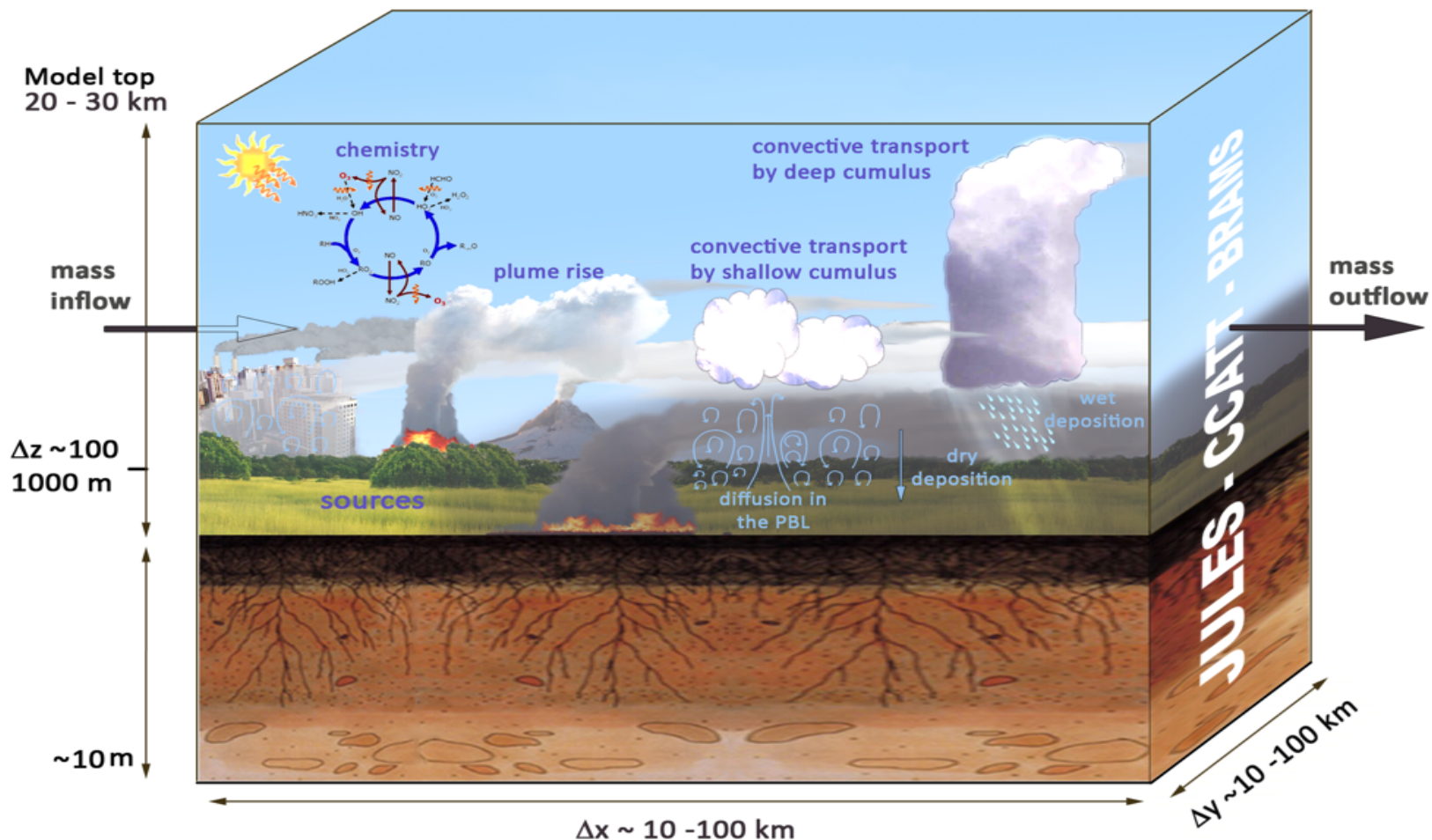
Using the Firefly optimization method to weight an ensemble of rainfall forecasts from the Brazilian developments on the Regional Atmospheric Modeling System (BRAMS)

A. F. dos Santos¹, S. R. Freitas¹, J. G. Z. de Mattos¹, H. F. de Campos Velho², M. A. Gan¹, E. F. P. da Luz², and G. A. Grell³



BRAMS 5.2 (new version)

Air quality and weather prediction



BRAMS – New version 5.2

Geosci. Model Dev. Discuss., doi:10.5194/gmd-2016-130, 2016

Manuscript under review for journal Geosci. Model Dev.

Published: 7 June 2016

© Author(s) 2016. CC-BY 3.0 License.

Geoscientific
Model Development
Discussions
Open Access
EGU

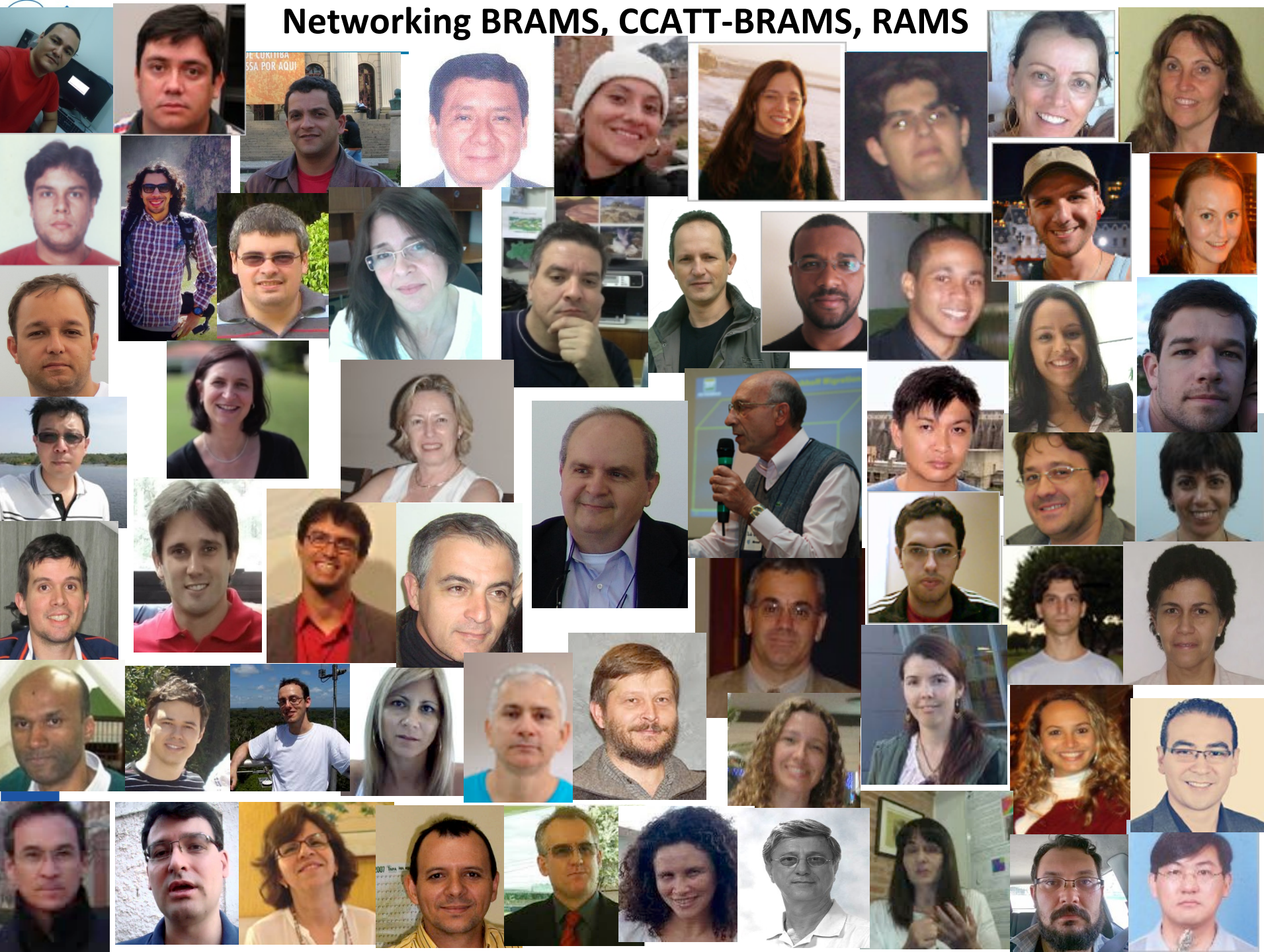


The Brazilian developments on the Regional Atmospheric Modeling System (BRAMS 5.2): an integrated environmental model tuned for tropical areas

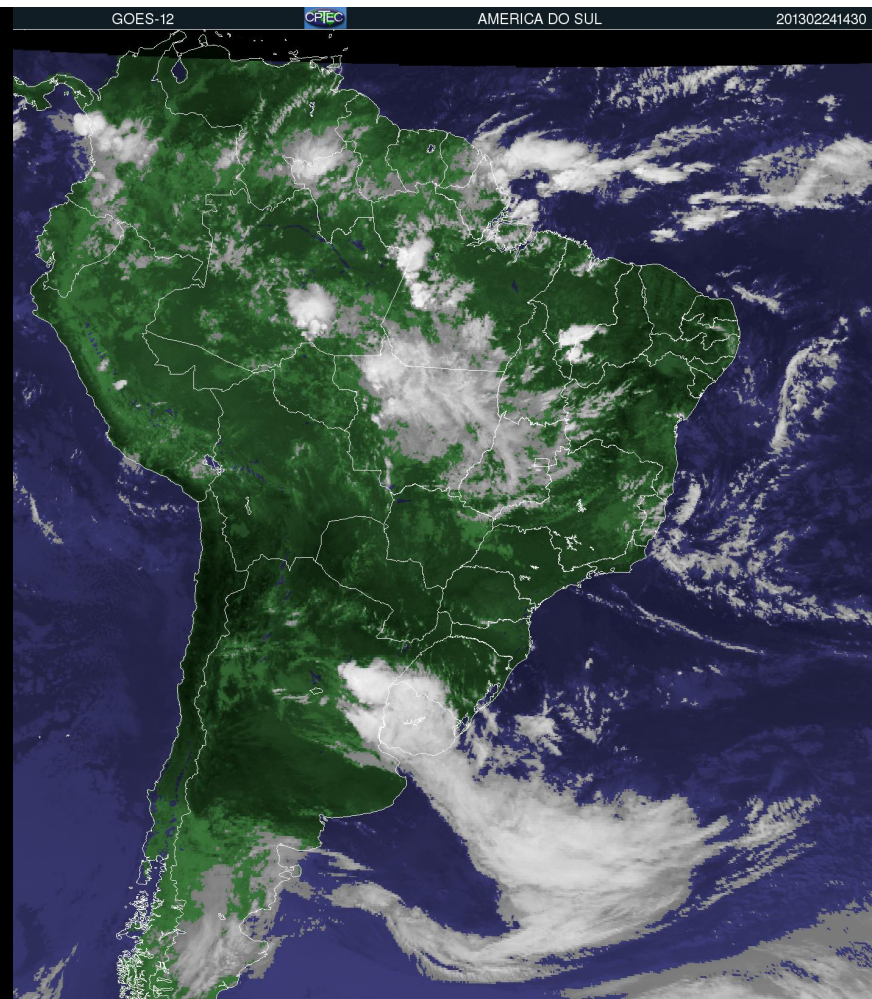
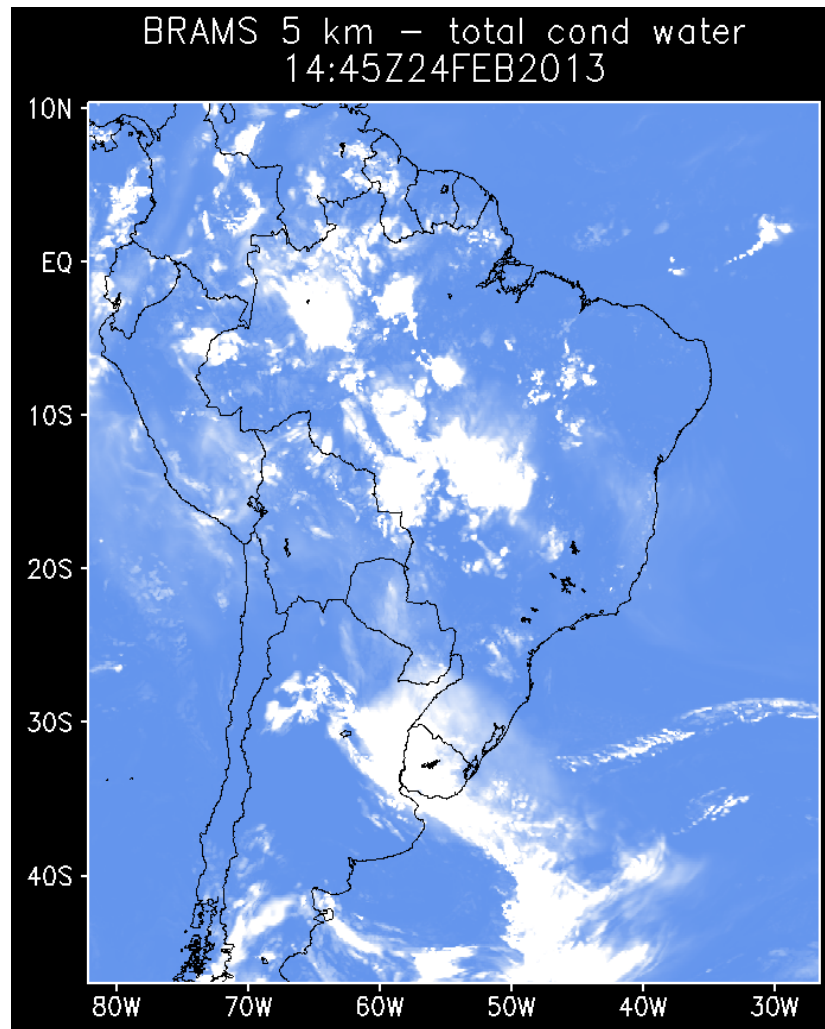
Saulo R. Freitas^{1,a}, Jairo Panetta², Karla M. Longo^{1,a}, Luiz F. Rodrigues¹, Demerval S. Moreira^{3,4}, Nilton E. Rosário⁵, Pedro L. Silva Dias⁶, Maria A. F. Silva Dias⁶, Enio P. Souza⁷, Edmilson D. Freitas⁶, Marcos Longo⁸, Ariane Frassoni¹, Alvaro L. Fazenda⁹, Cláudio M. Santos e Silva¹⁰, Cláudio A. B. Pavani¹, Denis Eiras¹, Daniela A. França¹, Daniel Massaru¹, Fernanda B. Silva¹, Fernando Cavalcante¹, Gabriel Pereira¹¹, Gláuber Camponogara⁵, Gonzalo A. Ferrada¹, Haroldo F. Campos Velho¹², Isilda Menezes^{13,14}, Julliana L. Freire¹, Marcelo F. Alonso¹⁵, Madeleine S. Gácita¹, Maurício Zarzur¹², Rafael M. Fonseca¹, Rafael S. Lima¹, Ricardo A. Siqueira¹, Rodrigo Braz¹, Simone Tomita¹, Valter Oliveira¹, Leila D. Martins¹⁶



Networking BRAMS, CCATT-BRAMS, RAMS



BRAMS 5.2 for weather prediction



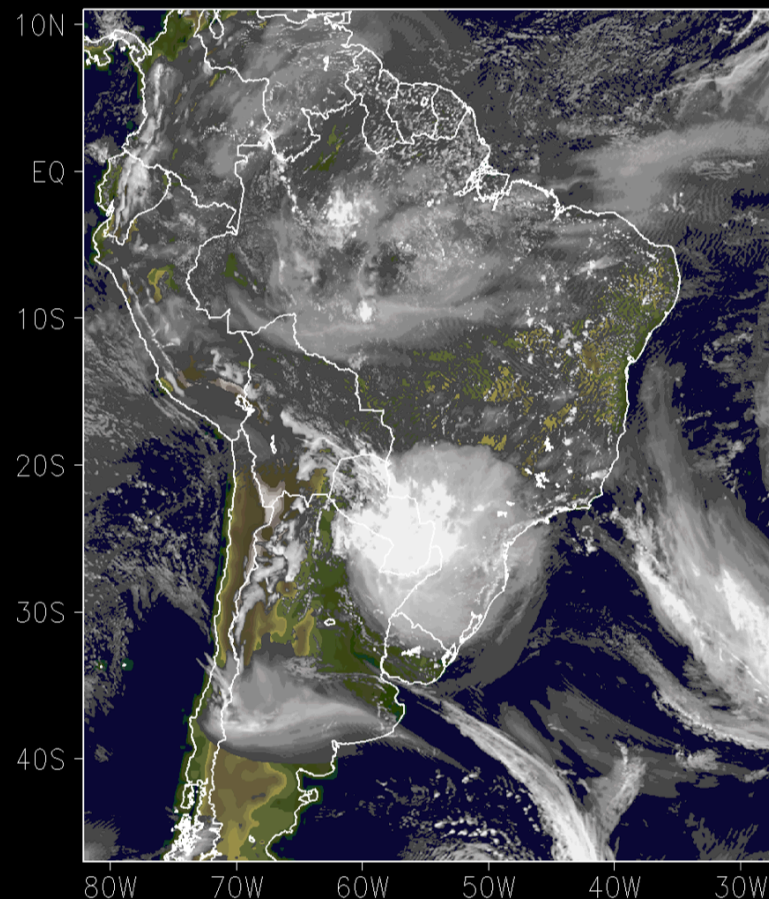
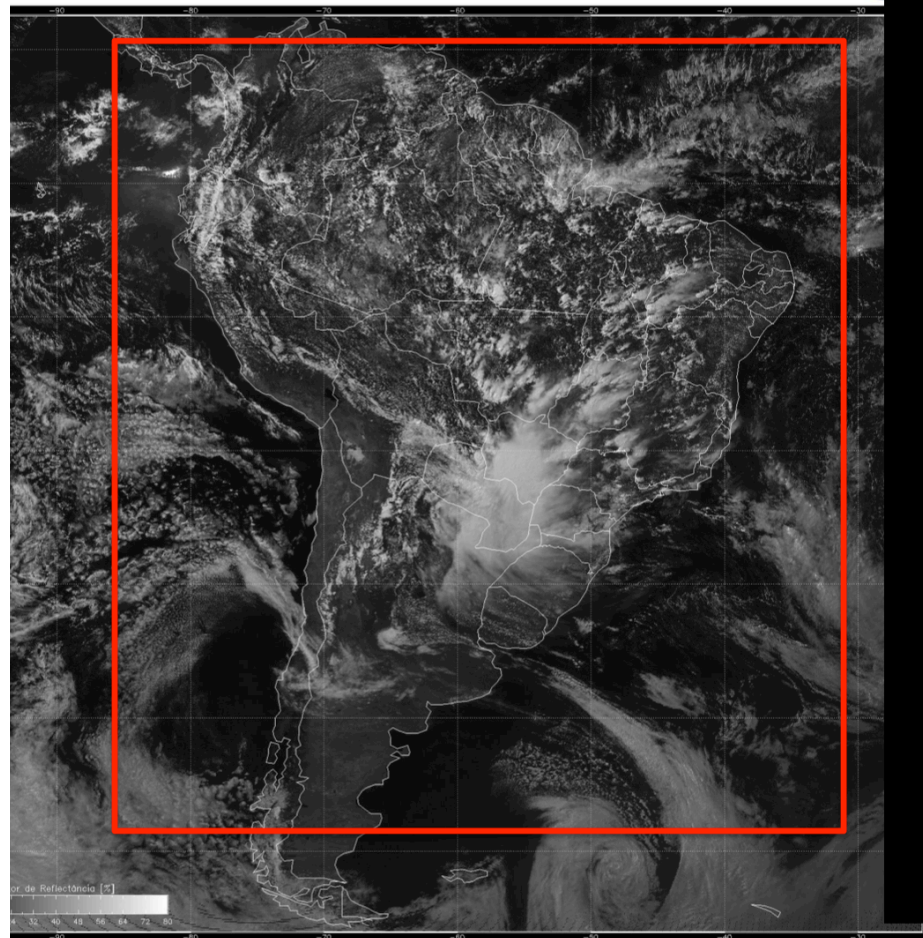
BRAMS 5.2 for weather prediction

ível (0.65 μm)
 Ul: 20160324 1800 GMT

CENTRO DE PREVISÃO DE
 TEMPO E ESTUDOS CLIMÁTICOS

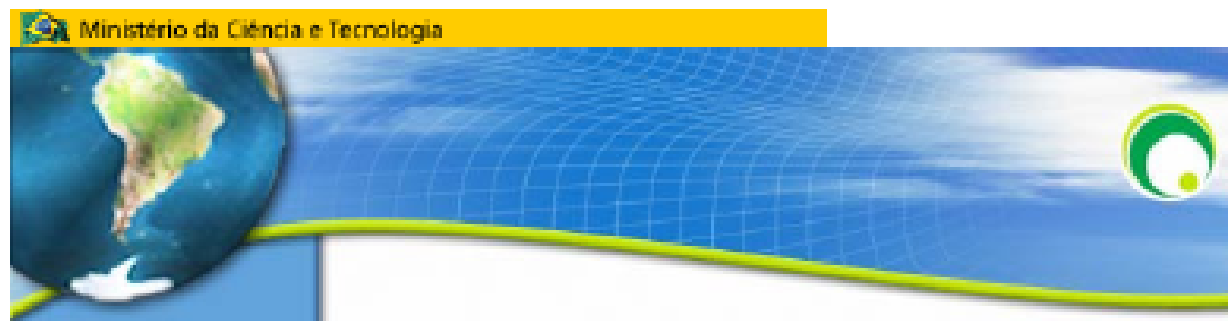


BRAMS 5km – total cond water 18Z24MAR2



B-RAMS is a free software

<http://brams.cptec.inpe.br>



E-mail:

Pwd:

[»Forgot your password?](#)
[»New Register here.](#)

- [» Home](#)
- [» News](#)
- [» Download](#)
- [» Screenshots](#)
- [» Projects](#)
- [» Press Release](#)
- [» Documentation](#)
- [» Papers, Thesis & Presentations](#)
- [» Skill against Observations](#)
- [» Bugzilla](#)
- [» Users RAMSIN](#)
- [» Links](#)
- [» Mailing list](#)



Model Description

Brazilian Regional Atmospheric Modeling System (BRAMS)

BRAMS (Brazilian Regional Atmospheric Modeling System) is a joint project of [ATMET](#), [IME/USP](#), [IAG/USP](#) and [CPTEC/INPE](#), funded by [FAPESP](#) (Funding Agency), aimed to produce a new version of [RAMS](#) for the tropics. The main objective is to provide a single model to Brazilian Weather Centers. The BRAMS/RAMS model is a multipurpose prediction model designed to simulate atmospheric circulation scale from hemispheric scales down to large eddy simulation: planetary boundary layer.



BRAMS is licensed under the [CC-GNU GPL](#).

BRAMS Version 3.2 is RAMS Version 5.04 plus:

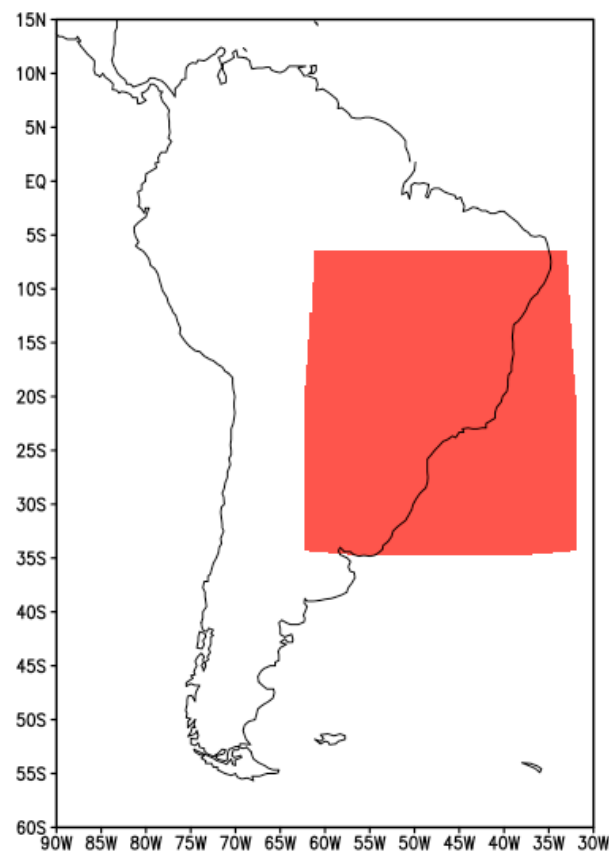
- Shallow Cumulus and New Deep Convection (mass flux several closures, based on Grell et al., 2002)

BRAMS 5.2 with 3rd Runge-Kutta

- Testing with 48 h of simulation
- Horizontal resolution: $\Delta x = \Delta y = 20$ km
- Weather condition: rain-fall under CZSA.
- Initial and boundary conditions:
from CPTEC-INPE AGCM: T126L28
T126: truncation at wave number 216
L28: vertical levels considered

BRAMS 5.2 with 3rd Runge-Kutta

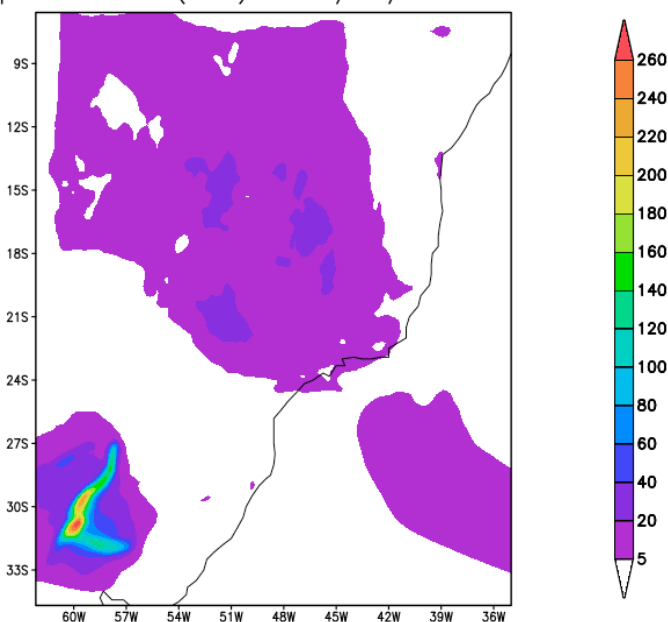
- Simulation domain



BRAMS 5.2 with 3rd Runge-Kutta

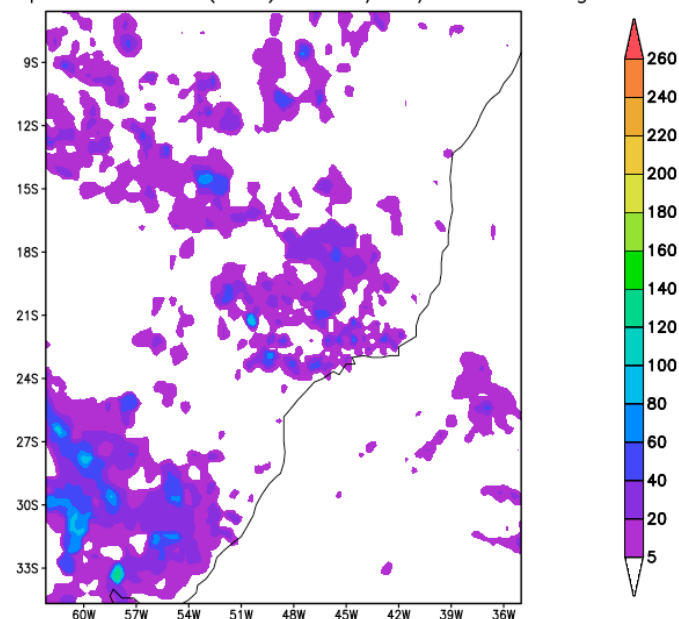
- Precipitation fields: RK3 ($\Delta t = 45$ sec)

Precipitacao 24h (mm) – 16/01/2017: RK-dt45



GrADS/COLA

Precipitacao 24h (mm) – 16/01/2017: Merge

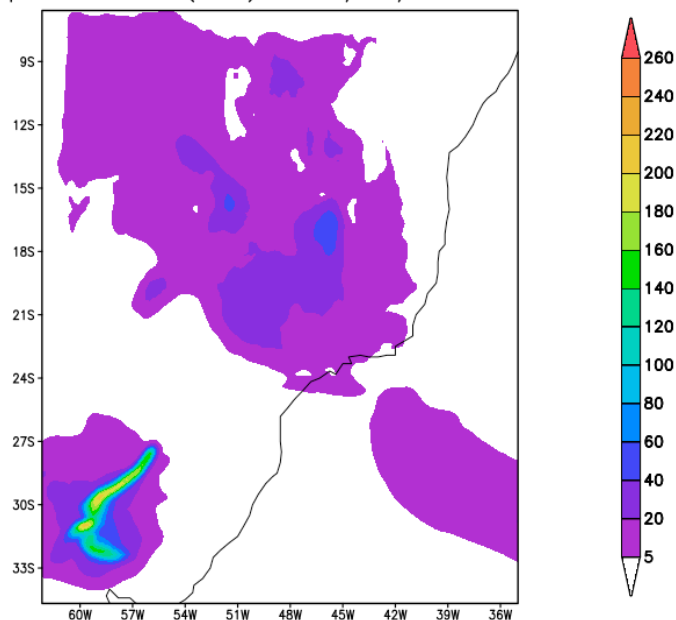


GrADS/COLA

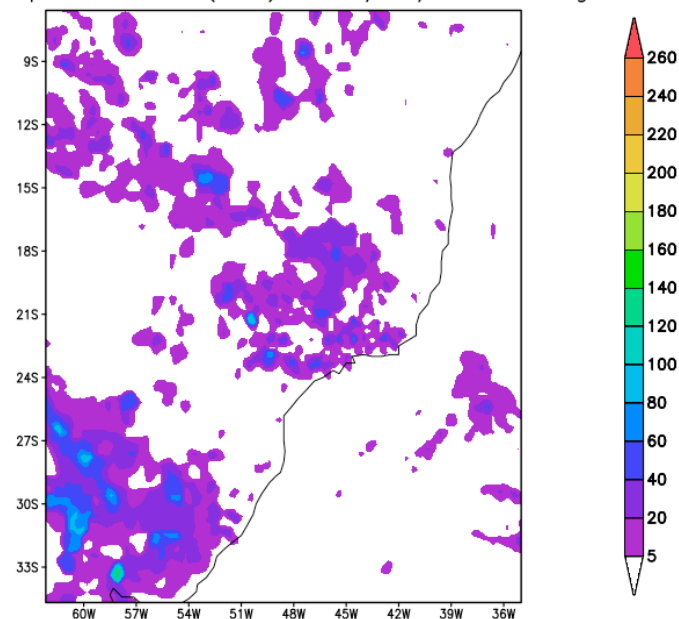
BRAMS 5.2 with 3rd Runge-Kutta

- Precipitation fields: LF ($\Delta t = 45$ sec)

Precipitacao 24h (mm) – 16/01/2017: LF-dt45



Precipitacao 24h (mm) – 16/01/2017: Merge

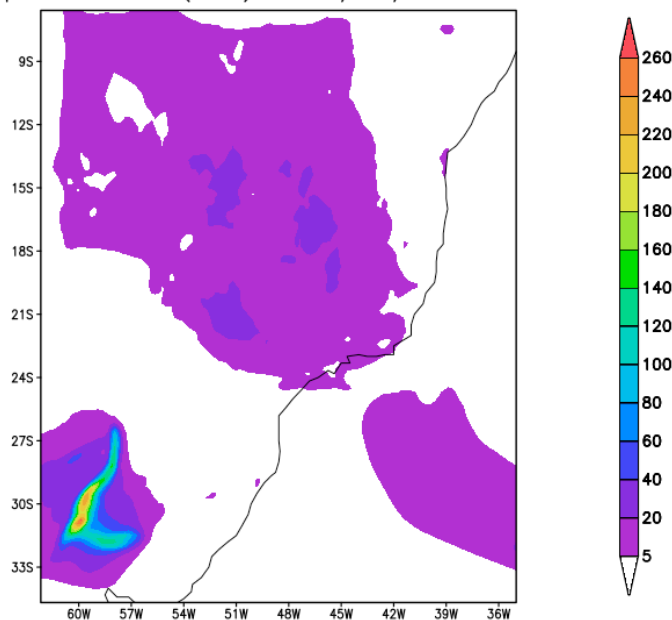


A

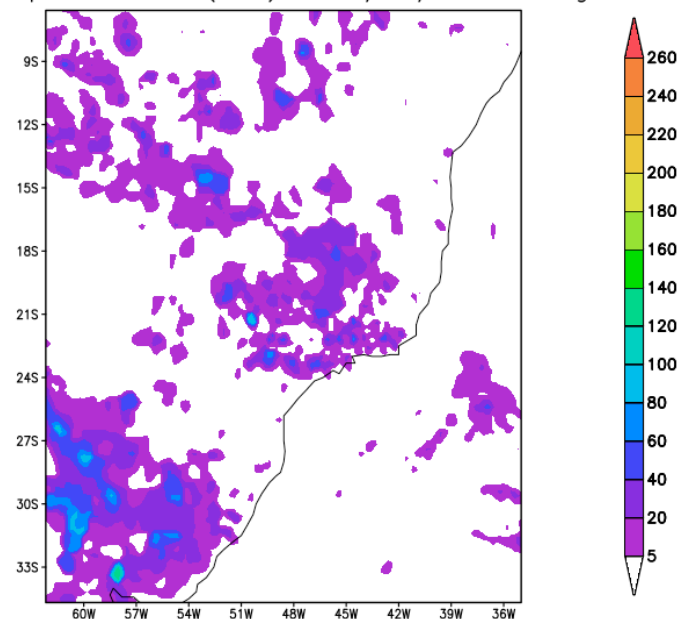
BRAMS 5.2 with 3rd Runge-Kutta

- Precipitation fields: RK3 ($\Delta t = 60$ sec)

Precipitacao 24h (mm) – 16/01/2017: RK-dt60



Precipitacao 24h (mm) – 16/01/2017: Merge



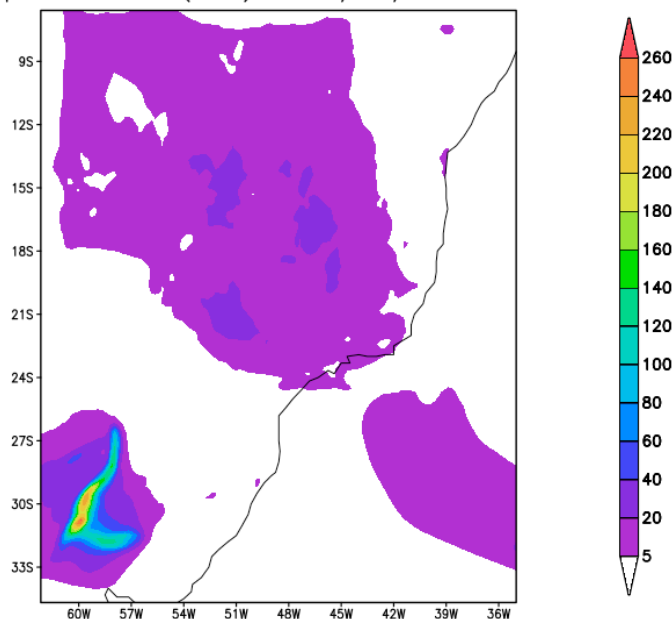
GrADS/OLA

OLA

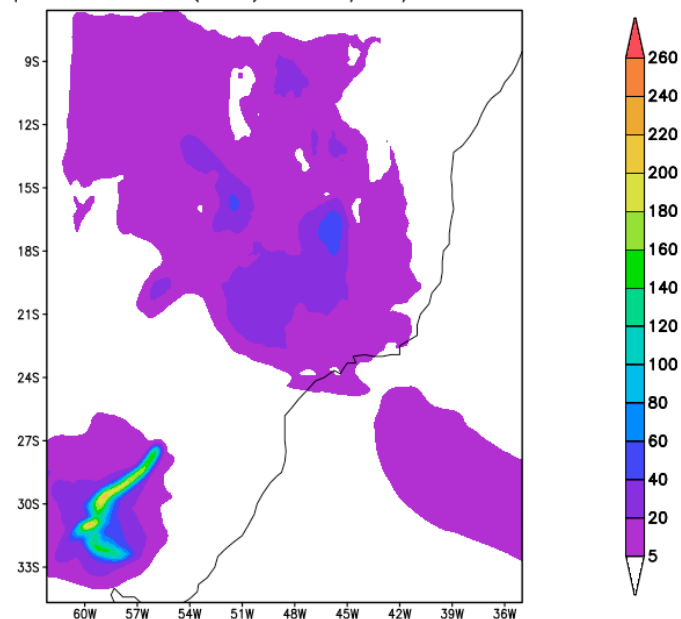
BRAMS 5.2 with 3rd Runge-Kutta

- RK3 ($\Delta t = 60$ sec) vs. LF ($\Delta t = 45$ sec)

Precipitacao 24h (mm) – 16/01/2017: RK-dt60



Precipitacao 24h (mm) – 16/01/2017: LF-dt45



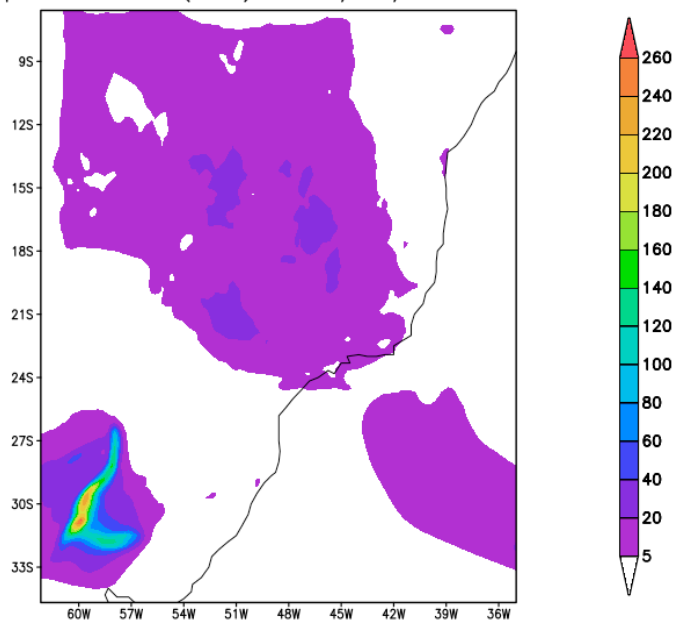
GrADS/COLA

GrADS/COLA

BRAMS 5.2 with 3rd Runge-Kutta

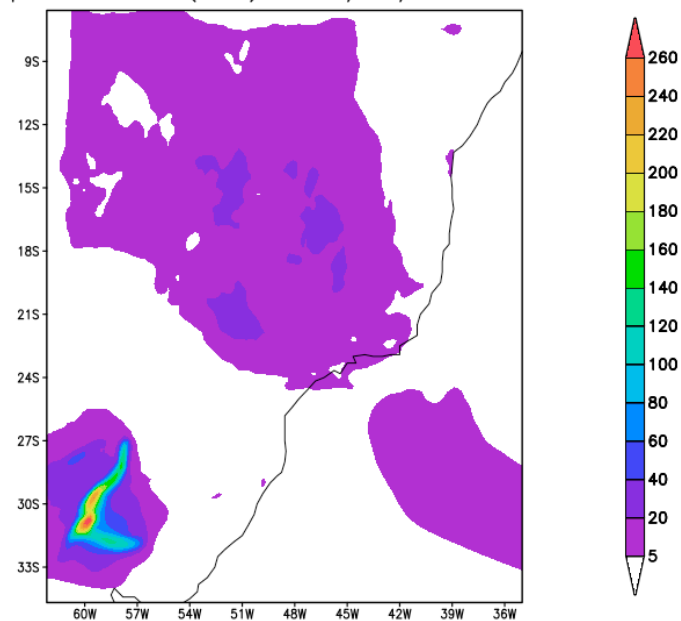
- RK3 ($\Delta y = 60$ sec) vs. RK3 ($\Delta t = 45$ sec)

Precipitacao 24h (mm) – 16/01/2017: RK-dt60



GrADS/COLA

Precipitacao 24h (mm) – 16/01/2017: RK-dt45



GrADS/COLA

Simulations comparisons: CZSA

- Rain-fall simulation under CZSA with BRAMS 5.2
- Runge-Kutta 3rd order was effective, and the stability condition was 1/3 larger then Leapfrog.

| | ZCAS | | |
|------|--------------|--------------|-------------|
| | RK3 (45s) | RK3 (60s) | LF (45s) |
| RMSE | 14.494 | 14.362 | 15.263 |
| VIES | 1.755 | 1.808 | 1.958 |

Simulations: El Niño, CZSA, ITCZ (not shown)

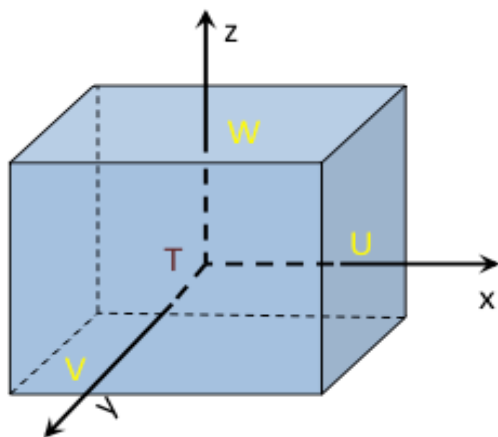
■ Other simulations

| | El Niño | | | ZCAS | | | ZCIT | | |
|------|--------------|--------------|-------------|--------------|--------------|-------------|--------------|---------------|-------------|
| | RK3 (45s) | RK3 (60s) | LF (45s) | RK3 (45s) | RK3 (60s) | LF (45s) | RK3 (45s) | RK 3 (60s) | LF (45s) |
| RMSE | 19.815 | 19.908 | 19.946 | 14.494 | 14.362 | 15.263 | 12.334 | 12.343 | 13.366 |
| VIES | -0.095 | 0.017 | -0.392 | 1.755 | 1.808 | 1.958 | 0.583 | 0.610 | 1.340 |

Parallel implementation

Arakawa grid-C

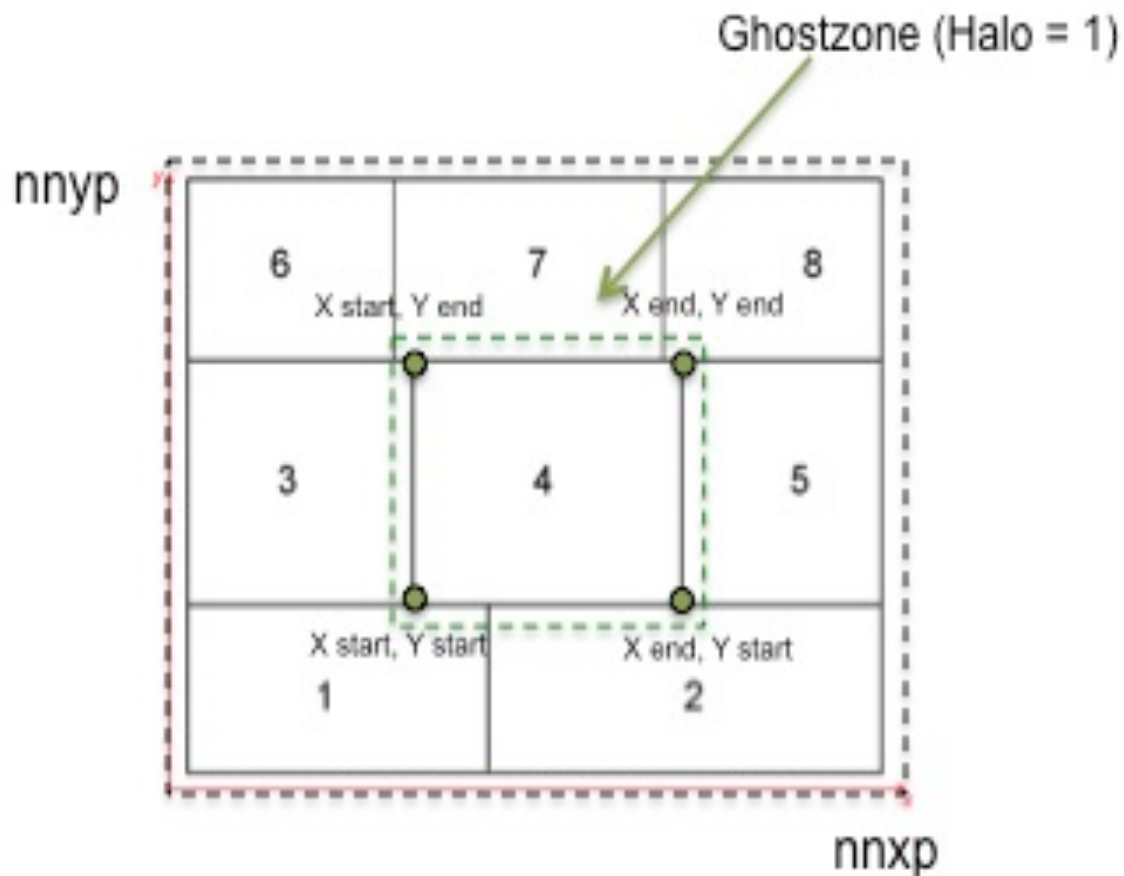
Velocity components and Temperature



| V_{18} | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | | |
|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{17} | | V_{27} | | V_{37} | | V_{47} | | V_{57} | | V_{67} | | V_{77} | | V_{87} | |
| T_{17} | U_{17} | T_{27} | U_{27} | T_{37} | U_{37} | T_{47} | U_{47} | T_{57} | U_{57} | T_{67} | U_{67} | T_{77} | U_{77} | T_{87} | U_{87} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | U_{78} | T_{88} | U_{88} |
| V_{18} | | V_{28} | | V_{38} | | V_{48} | | V_{58} | | V_{68} | | V_{78} | | V_{88} | |
| T_{18} | U_{18} | T_{28} | U_{28} | T_{38} | U_{38} | T_{48} | U_{48} | T_{58} | U_{58} | T_{68} | U_{68} | T_{78} | | | |

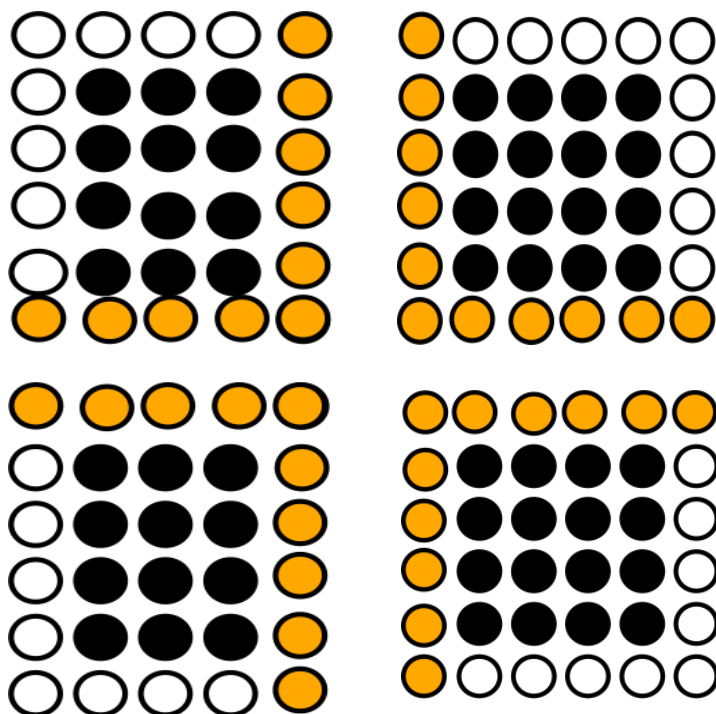
Parallel implementation

Strategy: independent domain decomposition



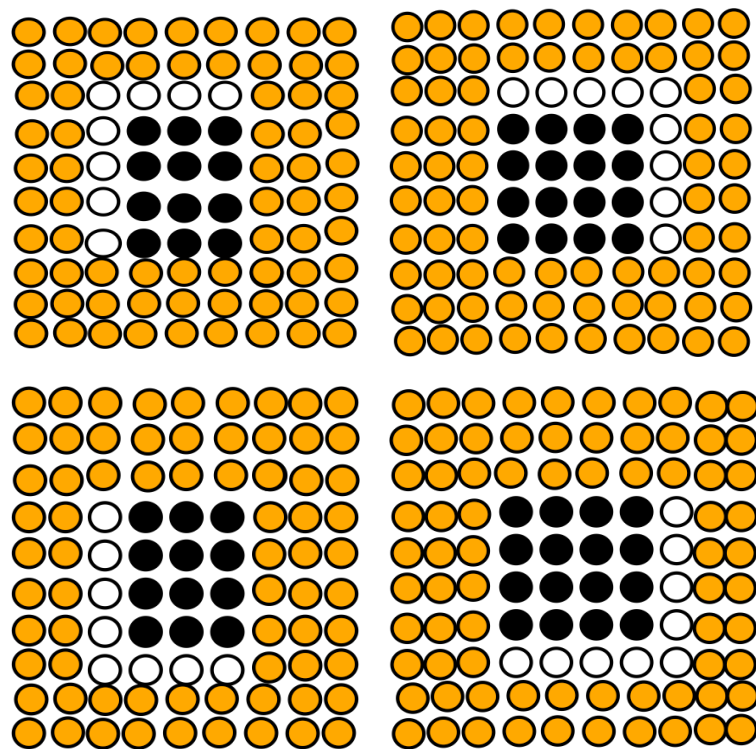
Parallel implementation

Strategy: old fashion - Leapfrog



Parallel implementation

Strategy: new approach – Runge-Kutta 3rd order



Cluster Lacibrido

**3 Nodes FPGA
(2014)**

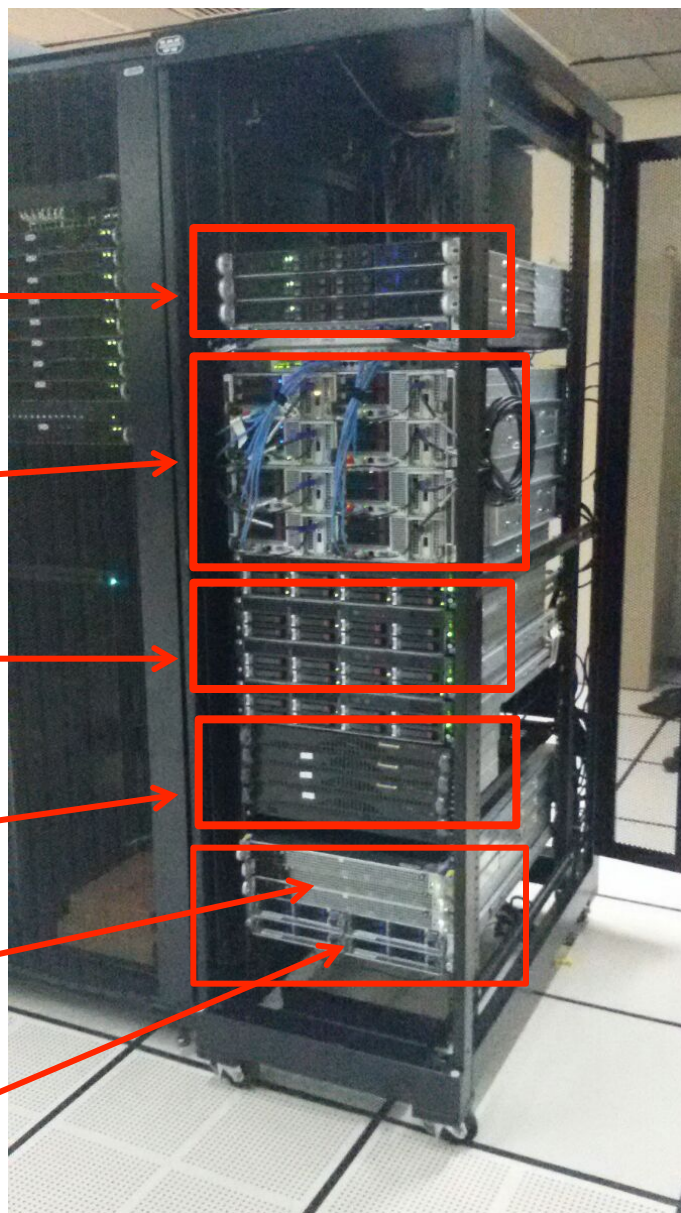
**8 Nodes 2013
(1, 2, ..., 7)**

**4 Nodes HP
(storage)**

**5 Nodes ARM
(2014)**

**3 Nodes FPGA
(2015)**

**4 Nodes ARM
(2015)**



Nodes 1,2, ..., 7 (2013):
2 proc. Intel 10-cores
2 GPU K20
FPGA Virtex-6

Nodes FPGA (2014):
2 proc. Intel 12-cores
GPU K20
Xeon Phi 60-cores
FPGA Virtex-7

Nodes FPGA (2015):
2 proc. Intel 12-cores
1 GPU K80
Xeon Phi (Knights Corner) 60-core
FPGA Virtex-7

Nodes ARM (2014):
5 AppliedMicro 8-core
(Calxeda: we can't buy)

Nodes ARM (2015):
8 Cavium ThunderX 48-cores

Parallel implementation – efficiency

BRAMS RK3: efficiently (Hybrid cluster – only CPU multi-core)

Table 1: BRAMS parallel execution evaluation to the RK3.

| Cores | CPU-time (sec) | efficiency |
|-------|----------------|------------|
| 10 | 27080 | — |
| 20 | 15661 | 72,91% |
| 40 | 7257 | 115,81% |
| 80 | 6895 | 5,25% |
| 120 | 4936 | 79,38% |
| 160 | 4150 | 56,82% |
| 200 | 3746 | 43,14% |
| 240 | 3330 | 62,46% |
| 280 | 3166 | 31,08% |



Final Remarks

1. Leapfrog (LF) and Runge-Kutta 3rd (RK3) order produced similar results to simulate the SACZ event. RK3 remain stable for a greater Δt than LF.
2. Other simulations with rainfall events (El Niño and ITCZ) obtained similar results.
3. Parallel version to the RK3 was effective. The code needed to be modified.
4. The performance for 40-cores (superlinear) and 80-cores (very poor) deserve to be more investigation.

Thank you!



Thank you!

CCIS 2019
5TH CONFERENCE OF COMPUTATIONAL INTERDISCIPLINARY SCIENCES

